

# Freeze-dryer Characterization: Execution and Application from Lab to Commercial

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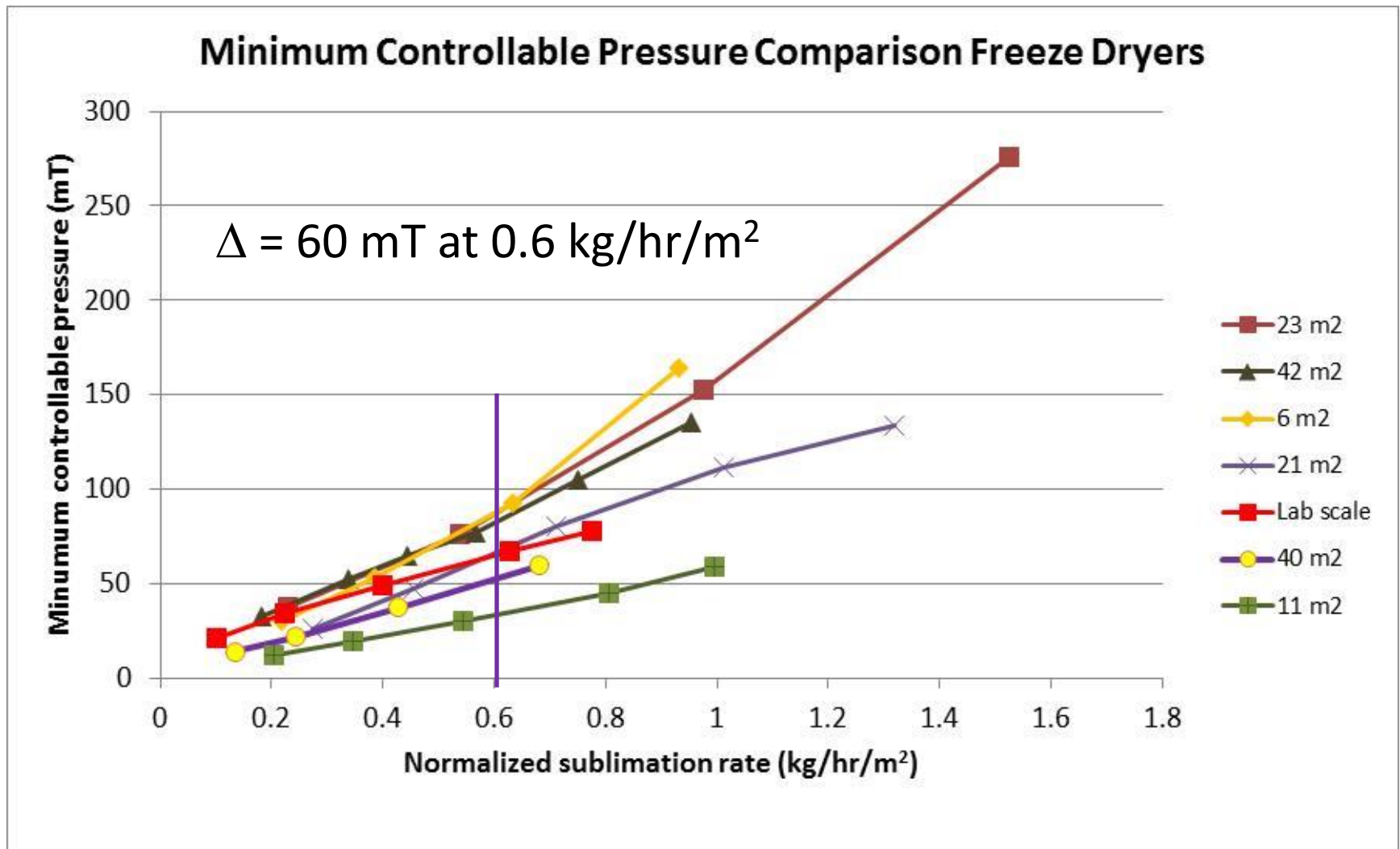
# Outline

- Define the purpose of characterization
- Methodology
  - Minimum controllable pressure as a function of sublimation rate
  - Maximum sublimation rate
  - Vial heat transfer coefficient ( $K_v$ )
- Application of data: Primary drying model
  - How are the data used?
  - What value does it have?
- Examples of Challenges

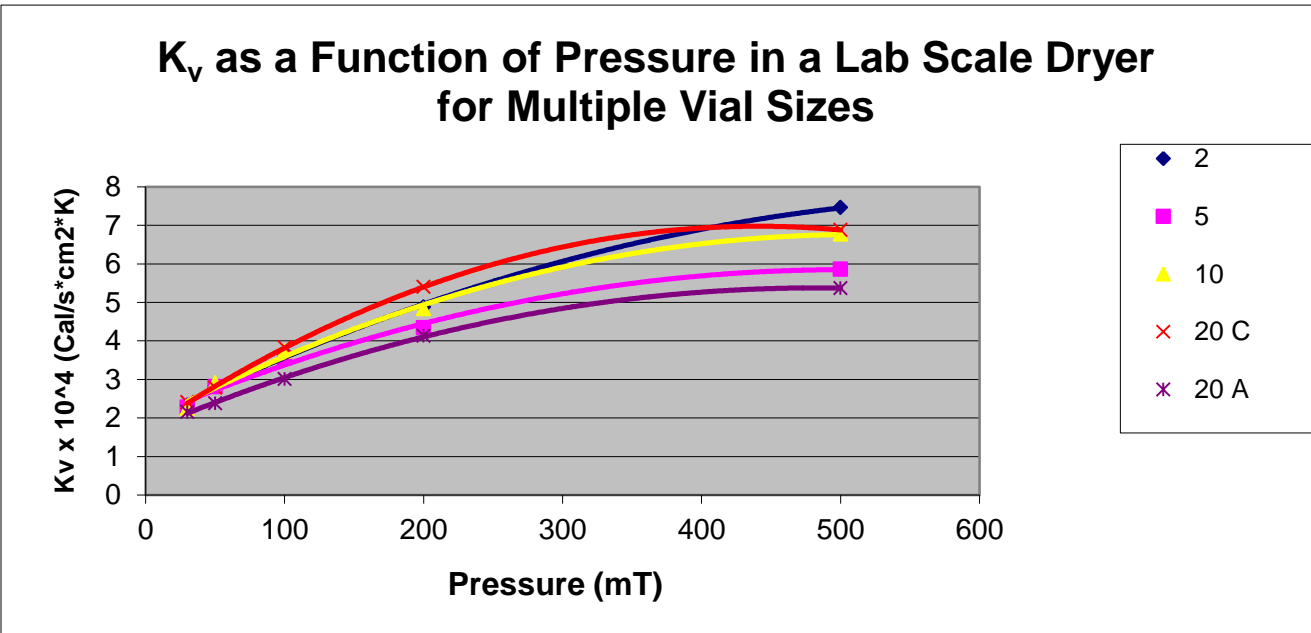
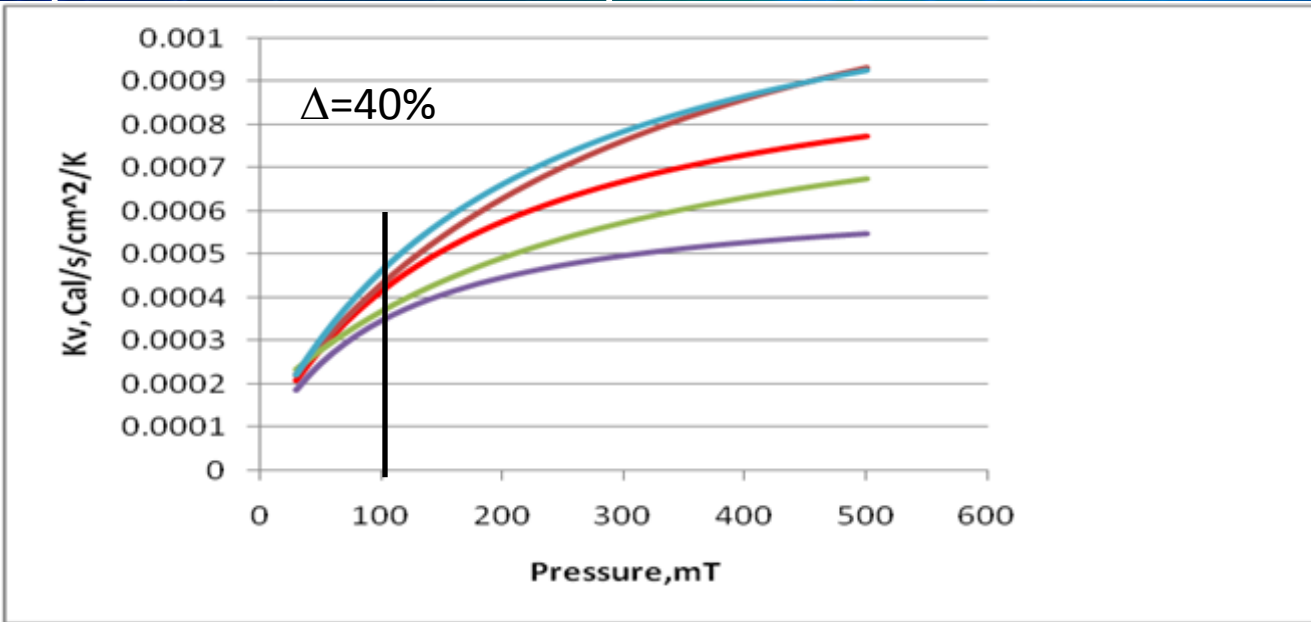
# Purpose of Lyo Characterization

- Generate data for the Pfizer 1° drying model
  - Facilitate cycle design and scale up/transfer
- Mission to characterize all dryers in network
- Physical differences in lyophilizers
  - Shelf size/thickness
  - Utilities
  - Environment
- Functional differences
  - $K_v$
  - Cake resistance
- If a development cycle was transferred to a commercial dryer without modification, it ~~could~~ would fail

# Differences: Minimum Controllable Pressure (MCP)



# $K_v$ Difference Between Laboratory, Pilot and Commercial Dryers (10-ml Schott vials)



# Minimum Controllable Pressure Test Execution

- Determine the lowest controllable chamber pressure as a function of sublimation rate
- Fully load the lyophilizer with water
  - Use vials
  - Bottomless trays with plastic
  - Trays with solid bottom
- Freeze water to -50 °C
- Pull vacuum to a minimum level (low set-point: 1-3 mT)
- Sequentially raise shelf temperature and hold until the chamber pressure equilibrates, target 25% mass loss (total)
- Calculate the sublimation rate at each shelf temperature
- Plot minimum controllable pressure as a function of sublimation rate

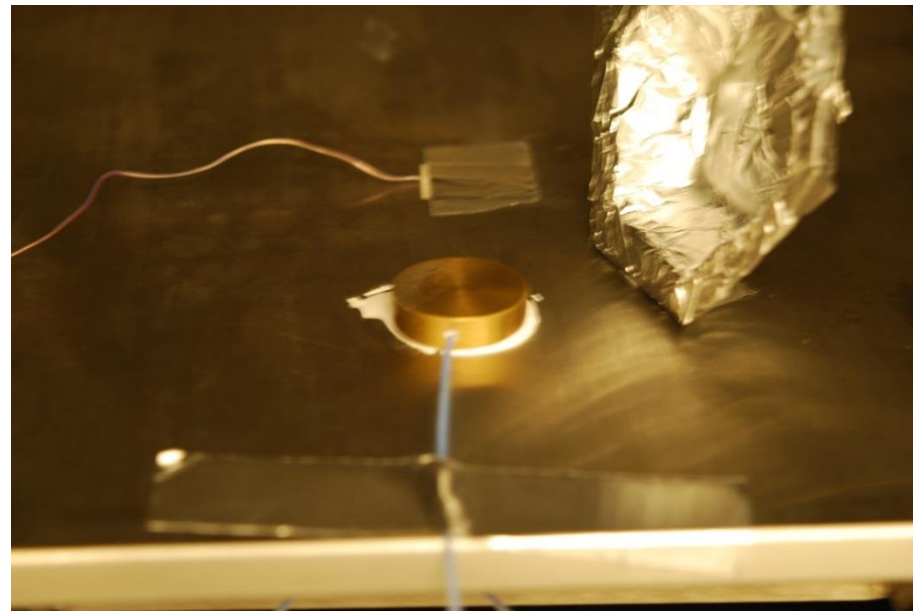
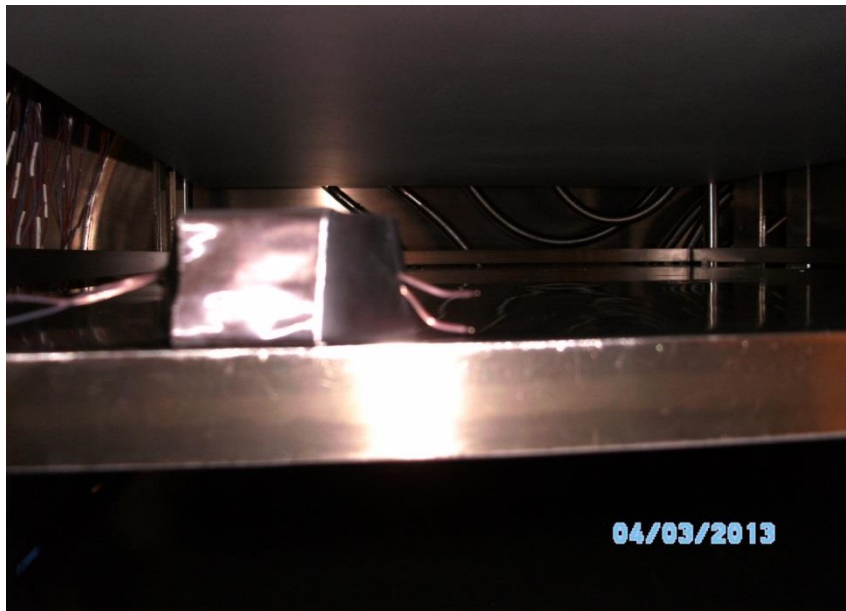
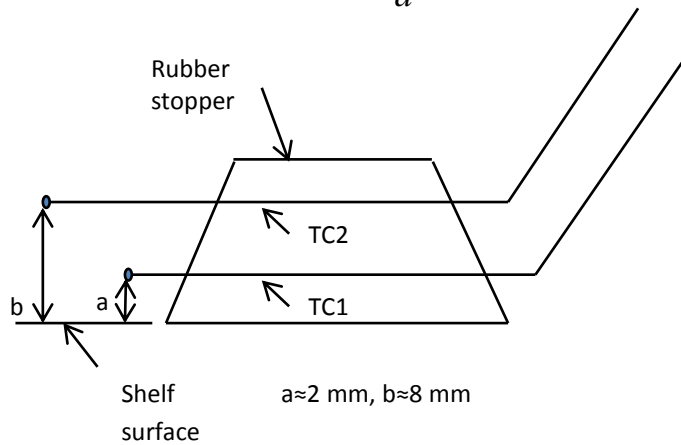


# Experimental Set-up: Clinical Scale



# Measuring Temperature: Ice and Shelf Surface

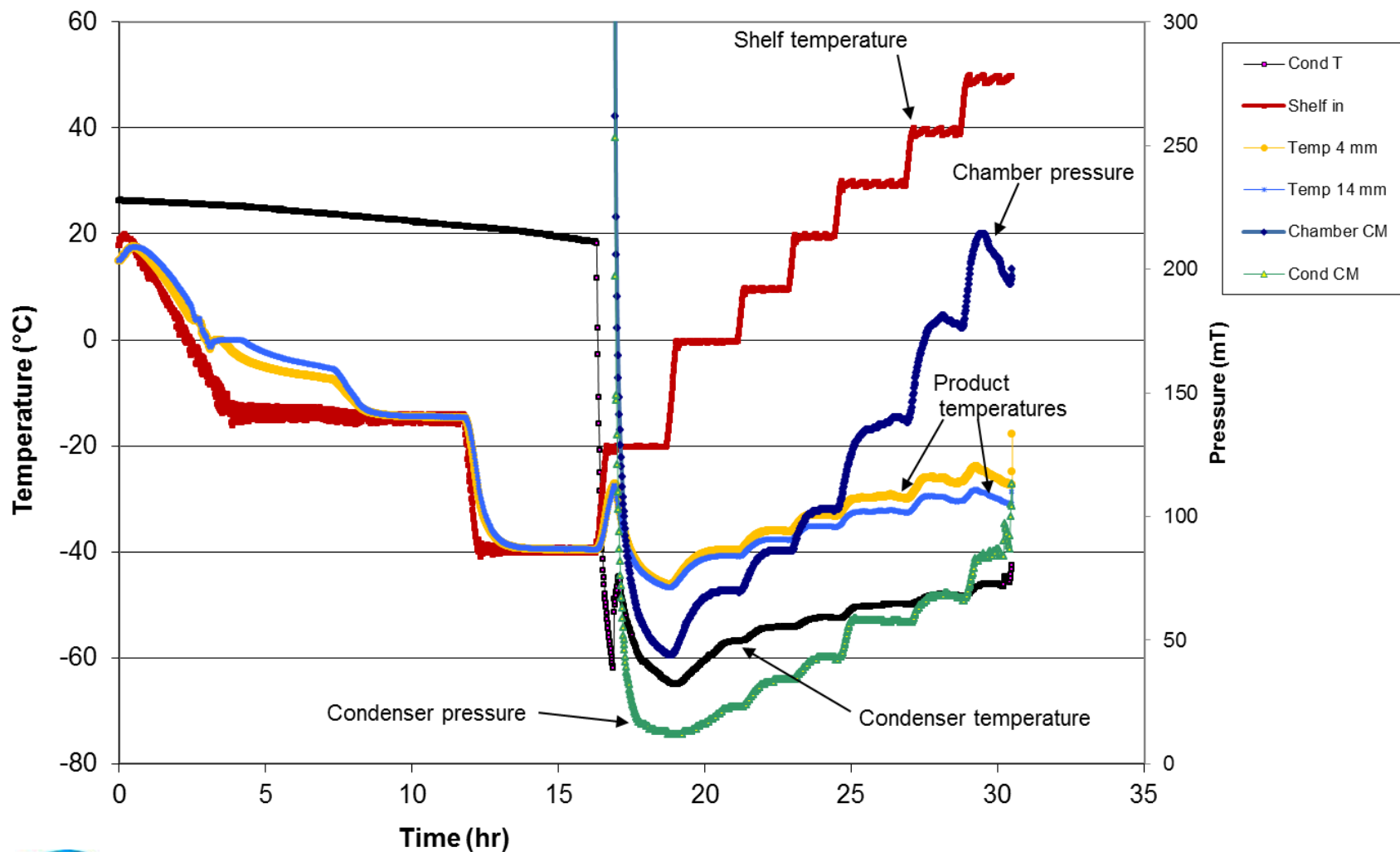
$$T_{ice\_bottom} = \frac{K_{bag} T_{shelf\_surface} + \frac{K_{ice}}{a} T_{ice}(a)}{K_{bag} + \frac{K_{ice}}{a}}$$





# Minimum Controllable Pressure Cycle

## Commercial Scale 42 m<sup>2</sup> Minimum Controllable Pressure



# Calculating Sublimation Rate

- Sublimation rate can be calculated over each time interval by:

$$\frac{dm}{dt} \left( \frac{kg}{hr * m^2} \right) = K_{cont} B (T_{shelf\_surface} - T_{ice\_bottom})$$

Where:

$K_{cont}$  is the container heat transfer coefficient, Cal/s/cm<sup>2</sup>/K;

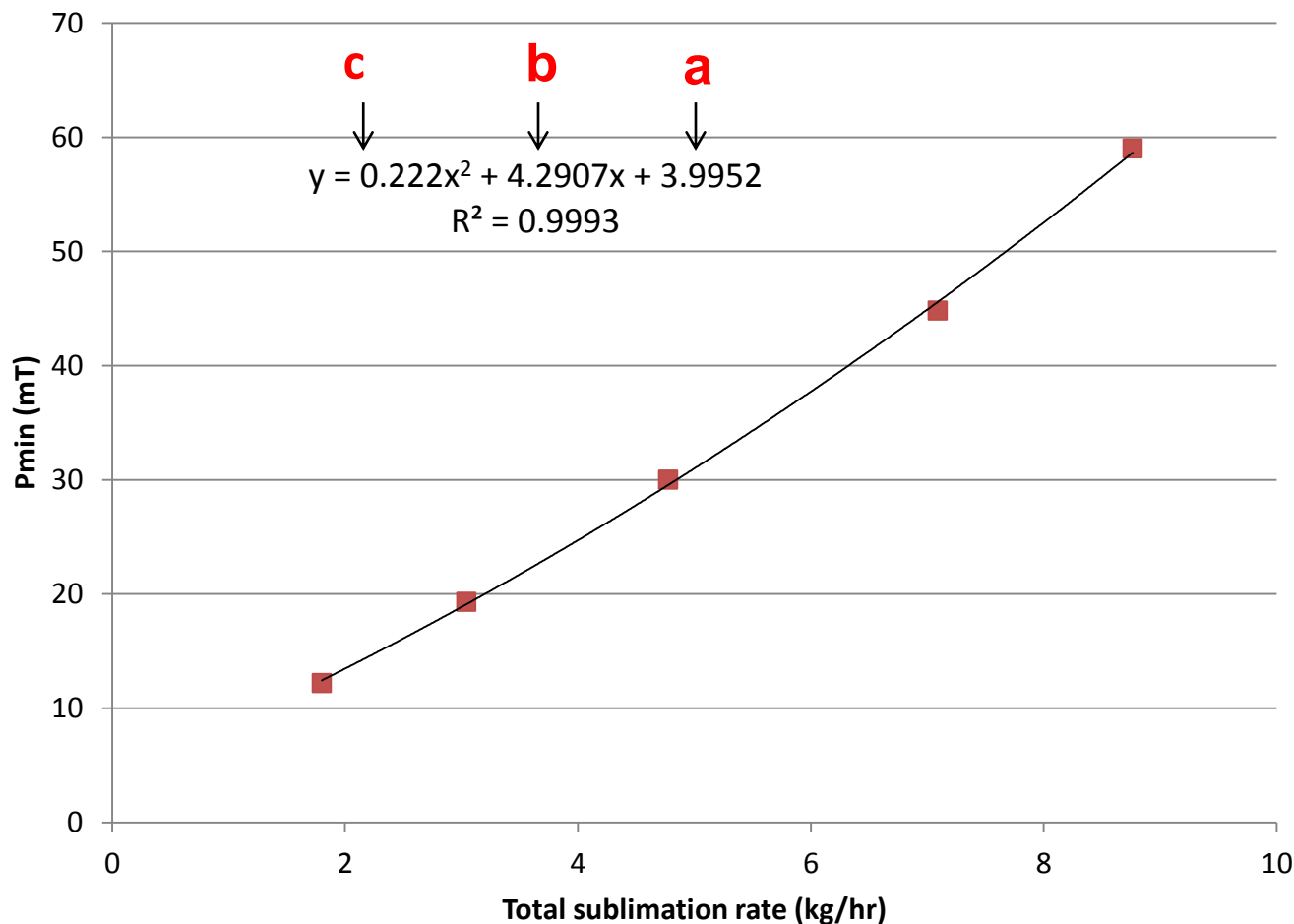
$B=53.25$  is a unit conversion coefficient;

$T_{shelf\_surface}$  is the average temperature of the shelf surface, °C;

$T_{ice\_bottom}$  is the temperature of the ice at the bottom of tray, °C.

# Minimum Controllable Pressure as a Function of Sublimation Rate

## Clinical Scale Minimum controllable Pressure



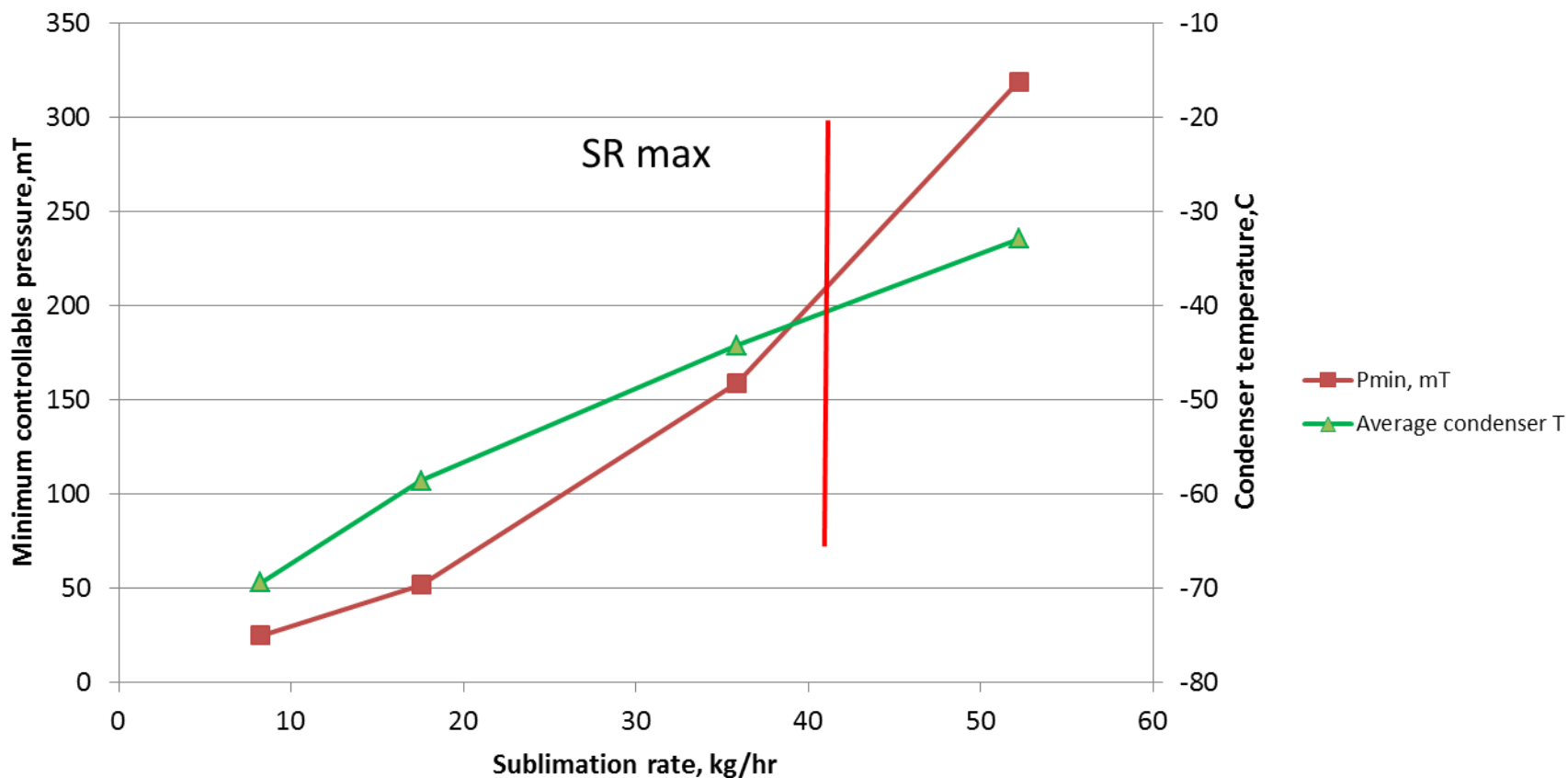
**Coefficients a, b and c are inputs in the model for P<sub>min</sub>**



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# Maximum sublimation rate ( $T_{\text{cond}} > -40^{\circ}\text{C}$ )

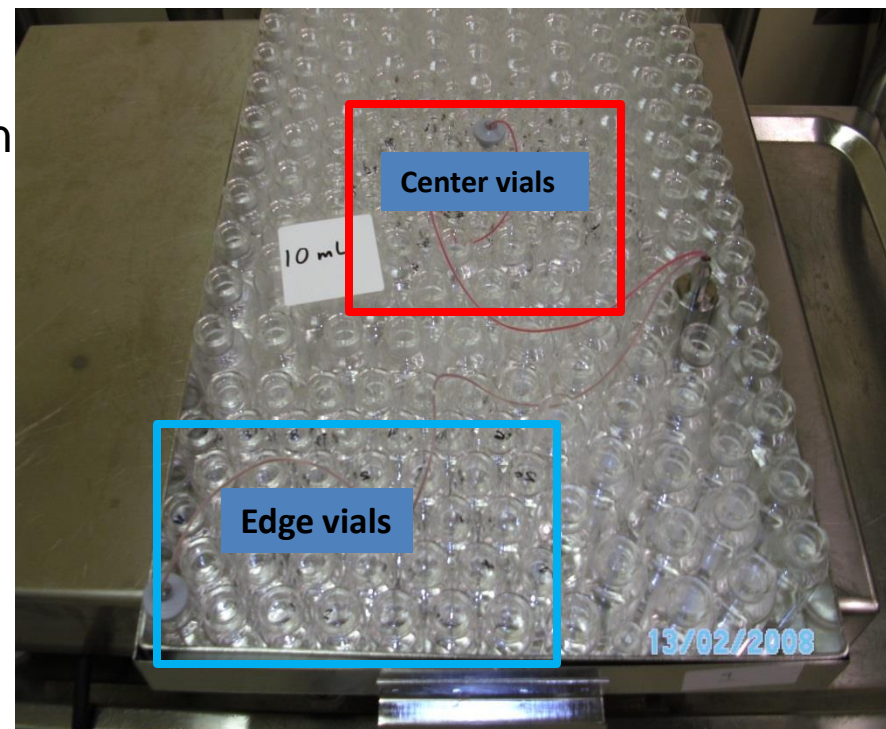
## Commercial Scale Maximum Sublimation Test



Condenser temperature exceeded  $-40^{\circ}\text{C}$  at sublimation rate  $\sim 42$  kg/hr  
(number to enter as  $\text{SR}_{\text{max}}$  into model)

# Vial Heat Transfer Coefficient Measurement

- Test calculates vial heat transfer coefficient at a single pressure
- Must perform multiple tests to determine heat transfer coefficient as a function of pressure
- Procedure:
  - Tare vials, add water to ~1 cm height, weigh
  - Set of vials at a front corner and a set of vials in the center
  - Use multiple vial sizes each run
  - Freeze, pull vacuum, ramp 1°C/min to 0°C and desired pressure
  - Hold ~ 2 hr for 100 mT, adjust time for other pressures
  - Target 25% mass loss, end cycle
  - Weigh to determine mass loss
  - Calculate  $K_v$  ( $dm/dt = K_v A \Delta T$ )





# Commercial Scale $K_v$ : 680 Vials (x2)

